

# EUR 2624.e

EUROPEAN ATOMIC ENERGY COMMUNITY — EURATOM

## A ONE-GROUP COLLISION PROBABILITY CODE FOR CYLINDERS AND SLABS

by

B. QUIQUEMELLE

1966



Joint Nuclear Research Center  
Ispra Establishment — Italy  
Reactor Physics Department  
Reactor Theory and Analysis



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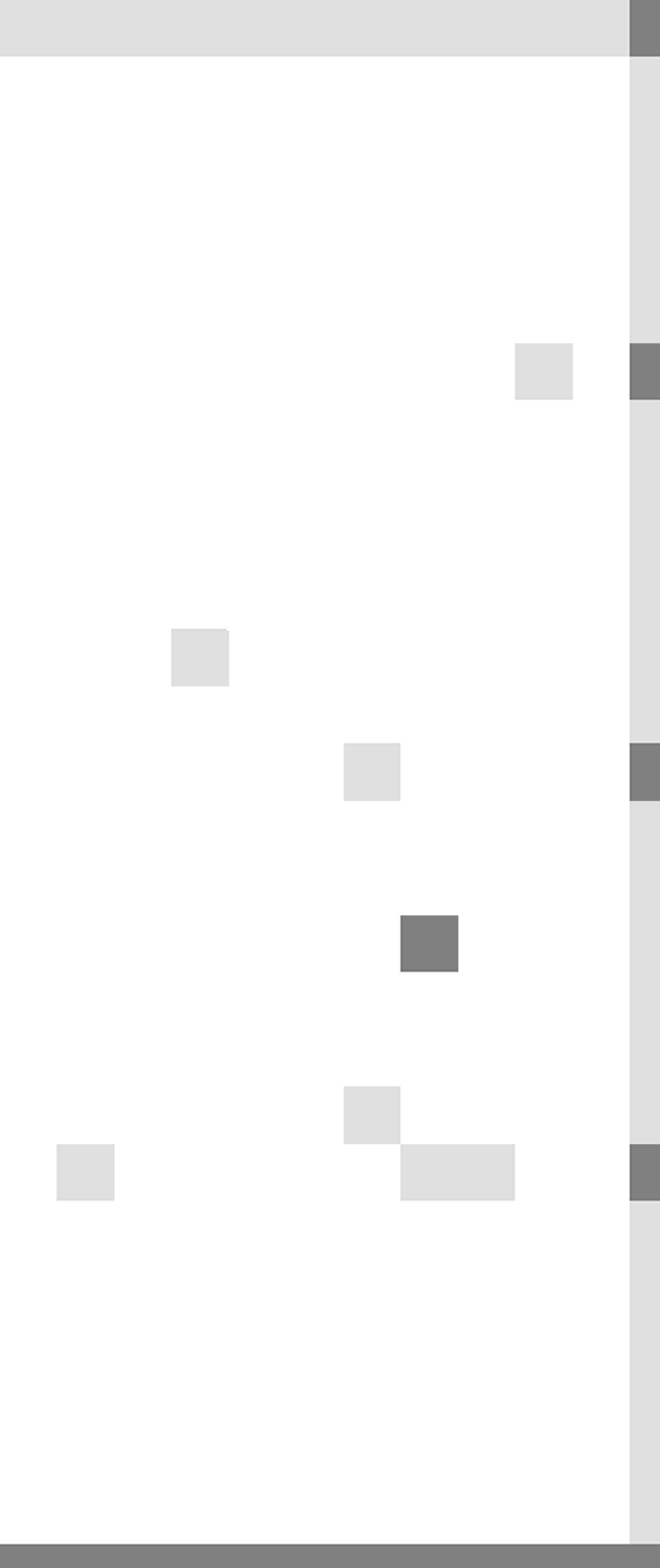
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## Summary

The Code <sup>0000</sup> forms the numerical evaluation of the collision probabilities in concentric spheres or slabs. For cell calculations several boundary conditions can be included including a black inner region. Escape probabilities and Dancoff coefficients calculations are compared with other methods. The complete list of the FORTRAN programme is given.

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### A one-group collision probability code for cylinders and slabs

#### Part I : Description of the method

##### Introduction (°)

In solving practical problems of neutron transport, the first flight collision probability theory has been proved successful since already some years. This theory provides a link between the most powerful methods for calculating the slowing down and the spatial distribution of neutrons.

Several works have dealt the analytical evaluation of collision probabilities in the simplest geometries. It has been thought interesting to solve the problem in using a straightforward numerical technique. Useful conclusions can then be drawn on the validity of such numerical techniques by comparison with the exact analytical evaluation

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(°) Manuscript received on November 5, 1965

### Method of Calculation

We will consider now a reactor or a lattice cell which can be represented by a one-dimensional geometry. Those geometries are formed of concentric cylinders or side by side slabs; also if we consider a regular lattice, the periodic structure will be taken into account by a suitable boundary condition.

We want to calculate the probability  $P_{R_i \rightarrow R_j}$  that a neutron born in a region " $R_i$ " - with a given space-angle distribution - collides in a region " $R_j$ ". In case of a regular lattice,  $R_i$  refers to a well defined region of the cell together with the homolog region in the other cells (through a suitable cell boundary condition).

Considering a normalized source of neutron in region " $R_i$ " and the corresponding first flight collision flux  $\phi$ , the quantity to be calculated is just

$$P_{R_i \rightarrow R_j} = \int_{R_j} \phi(r) \Sigma_t(r) dr$$

where  $\Sigma_t$  is the total cross section at space point  $r$ .

Such a problem is easily solved by the numerical integration of the inhomogeneous Boltzmann equation using the so-called " $S_n$  approximation". This approximation consists in the discretisation of the angular and space variables. A mesh cell is then specified by an index  $i$  for the space variable and two indices  $l, m$  for the direction of flight vector. One then considers<sup>1</sup> the value of the flux on each boundary of the mesh cell such as  $\phi_i$  which is the value at space point  $r_i$  (or  $x_i$ ) when the direction of flight is an averaged direction inside the mesh cell. Similar definitions<sup>1</sup> exist for  $\phi_m$  and  $\phi_l$ . A set of difference type equations is written between those values  $\phi_i$ ,  $\phi_m$  and  $\phi_l$  by representing the flux with an approximate shape inside the mesh cell.

In usual  $S_n$  calculations, this set is solved from mesh cell to mesh cell by starting with known conditions on the boundary of the system, then solving the equations by recursion and iterating until a conver-



gence criterium is reached. In our case we are interested in the collision probabilities for which the medium is considered to be absorbing for all types of collisions. Then no iteration is needed which avoid the most time consuming operations of the usual  $S_n$ .

Without going in any more details the main equations solved by the code have been gathered in appendix I.

If the calculation is done inside one cell of a lattice, the contributions from other cells are introduced through a balance equation at the external boundary

$$\vec{\Phi}_I = R \cdot (\vec{g}_I + T \cdot \vec{\Phi}_I)$$

The vectors have for components the flux along the discrete directions chosen for the mechanical quadrature. It is really this balance equation which avoids the iteration over the space mesh and which suppresses the need for the inner iteration of the usual  $S_n$  codes.

- $\vec{g}_I$  represents the neutrons coming directly from the source and leaving the lattice cell without having collided.
  - $\vec{\Phi}_I$  represents the neutrons coming from the other cells in the lattice.
  - $T$  is the transmission matrix of the lattice cell for incoming neutrons. When the set of discrete directions is symmetric for inward and outward directions this matrix is diagonal. In this case the elements of the matrix  $T$  are found in solving the system of equations of appendix I for an isotropic boundary source of unit intensity and collecting the number of neutrons leaving the cell along discrete outward directions.
- The elements of the matrix  $R$  represent the coefficients of transfer from one outward direction to one inward direction.

The result of the calculation is just a square matrix of the  $P_{R_i \rightarrow R_j}$  which we will write more simply  $P_{ij}$ . The elements of this matrix must satisfy the reciprocity relations

$$V_i \lambda_j P_{ij} = V_j \lambda_i P_{ji}$$

and also the conservation relations (in an infinite lattice)

$$\sum_j P_{ij} = 1$$

where  $V$  and  $\lambda$  are the volume and mean free path inside the region designated by the subscript. It should be noted that those relations are already a very good check for the accuracy of the numerical method.

### Conclusion

This method for calculating the collision probabilities is fast and accurate. When used for a lattice geometry, rather complicated boundary laws are simply introduced through the specification of the  $R$  matrix. In the present code the neutrons are started uniformly and isotropically in each region but an extension has been done for dealing with anisotropic sources<sup>14</sup>. This code can also be used like a subroutine for calculating transport kernels with a flux calculation method similar to the THERMOS method<sup>12</sup>. It is thought that rather accurate kernels are found in a short time even for large size regions. The advantage of this method over the DSN method is that the  $S_n$  approximation is used only for calculating accurate transport kernels with a minimum effort, then well developed techniques for accelerating convergence are used to solve the linear flux equations<sup>12</sup>.



List of Symbols

$i$	index for designation of a space mesh boundary
$l, m$	two indices for designation of an angular mesh boundary
$\phi_k$	( $k = i, l$ or $m$ ) value of the flux on the boundary labelled by index $k$ when the variables which varies over other boundaries have a mean value <sup>3</sup>
$\sum_i$	total cross section inside space mesh $r_i, r_{i+1}$
$w$	weight associated to the discrete direction inside the mesh cell and used for mechanical quadrature (half value indices are generally omitted for clarity)
$\mu$	direction cosine
$r_i, r_{i+1}$	inner and outer radius of mesh $i$ in cylindrical geometry
$x_i, x_{i+1}$	abscissa defining the mesh $i$ in slab geometry
$P_{R_i \rightarrow R_j}$	probability that a neutron born uniformly and isotropically in region $R_i$ suffers his first collision in region $R_j$
$\delta_R$	is 1 inside the region $R$ and 0 outside
$I$	number of space mesh
$n$	order of approximation for the discrete angular representation In cylindrical geometry there exist $\frac{n(n+4)}{4}$ discrete direction and in slab geometry there exist $n$ discrete directions.

Part 2: Some applications of the code  
=====

The code has been applied to a variety of problems and results were compared with exact methods.

a) calculation of escape probabilities:

We consider, by example, a two-media cell in a lattice consisting of a fuel rod surrounded by a moderator. The probability of escaping the rod is just

$$P_o = P_{f \rightarrow m}$$

where  $P_{f \rightarrow m}$  is calculated using the code TIJ with two regions (fuel + moderator). Such a calculation is reported in table II and compared with other analytical methods. It should be noted that the best boundary condition is given by an isotropic return along directions which have the same azimuth that the incident neutron direction (although the difference with a purely isotropic return is negligible). In this case the results compared very closely with the analytic calculations of Pennington<sup>4</sup>. We can also state that there exists no simple specification for finding the exact results of Fukai<sup>5</sup> with any combination of two or three boundary laws.

In table III a similar calculation was performed and shows a very good agreement with Monte Carlo calculations reported by Rothenstein<sup>7</sup>.



Table II

## Escape Probabilities

(a (radius of rod) = 0.183 inch,  $v_m/v_f = 1.0$ ,  $\Sigma_m = 1.49170 \text{ cm}^{-1}$ )

$\Sigma_{fuel}^a$	Takahashi <sup>6</sup>	TIJ			Pennington <sup>4</sup>	exact <sup>5</sup>
		IBVL = 1	IBVL = 3	IBVL = 2		
0.1	0.76875	0.7723	0.8160	0.8157	0.81364	0.80745
0.3	0.52590	0.5295	0.5908	0.5898	0.58855	0.57988
0.5	0.39776	0.4014	0.4589	0.4575	0.45695	0.44745
0.8	0.28918	0.2927	0.3400	0.3383	0.33839	0.32973
1.0	0.24372	0.2471	0.2884	0.2866	0.28694	0.27918
2.0	0.12393	0.1358	0.1603	0.1588	0.15912	0.15490
4.0	0.068981	0.07047	0.08281	0.08196	0.082044	0.080363

\* approximation  $S_{16}$

IBVL = 1 (mirror reflection)

IBVL = 3 (white boundary)

IBVL = 2 (isotropic return along same azimuth)

Table III

## Escape Probabilities

$$(v_m/v_f = 1.0, \sum_m = 1.4916 \text{ cm}^{-1})$$

$\sum_{fuel}^a$	$TIJ^*$	Monte Carlo <sup>7</sup>	$TIJ^*$	Monte Carlo <sup>7</sup>
0.5	0.5750 (0.5631)	0.572 (0.553)	0.6950	0.691
1.0	0.3988	0.397	0.5243 (0.5159)	0.522 (0.513)
1.458	-	-	0.4237	0.422
1.5	0.3026 (0.2909)	0.304 (0.291)	-	-
2.0	0.2424	0.248	0.3422 (0.3343)	0.346 (0.335)
3.0	0.1718 (0.1636)	0.173 (0.163)	0.2491	0.250
4.0	0.1324	0.133	0.1939 (0.1883)	0.194 (0.190)
6.0	0.09017 (0.0851)	0.088 (0.082)	0.1330	0.133
8.0	-	-	0.1007 (0.0976)	0.100 (0.099)
	a = 0.25 inch		a = 0.60 inch	

\* approximation  $S_{16}$  with isotropic return  
 (values between parenthesis include the effect of a 0.033 in. cladding)



b) Dancoff factor calculations

It is possible to specify a black inner region in the cylindrical geometry. In this case TIJ code prints the current  $J_{in}^-$  of neutrons entering the black region. If we perform a two region calculation with a cell boundary condition (IBVL different of 0) we can calculate the shadowing factor of Dancoff:

$$C = J_{in}^- \times 4 \sum_m$$

where  $1/4 \sum_m$  is the current in the infinite moderator.

Such a calculation is reported on table IV and compared to exact Monte Carlo<sup>8</sup> calculations. There is a maximum discrepancy of 3.5% which can well be explained by the inadequacy of the linear approximation near the inner black boundary. It should be also necessary to use more discrete directions near the discontinuity of the angular flux at the black boundary. Those calculations compare well with some analytical results<sup>9</sup> but they are not as accurate as the Sauer<sup>10</sup> approximation.

Table IV

Dancoff coefficient

$$(\sum_m = 1.4916)$$

Rod size (inch)	$V_m/V_f$	IBVL = 1	TIJ IBVL = 2	IBVL = 3	Monte Carlo <sup>8</sup>
0.250	1.0	0.4532	0.5507	0.5400	0.52690
	1.5	0.5637	0.6797	0.6718	0.64627
	2.0	0.6342	0.7551	0.7472	0.73077
	3.0	0.7366	0.8514	0.8445	0.82361
	4.0	0.8026	0.9040	0.8983	0.88566
0.387	1.0	0.5960	0.6898	0.6820	0.66169
	1.5	0.7071	0.8023	0.7949	0.77261
	2.0	0.7751	0.8678	0.8619	0.84533
	3.0	0.8670	0.9357	0.9309	0.90732
	4.0	0.9252	0.9729	0.9697	0.95422
0.600	1.0	0.7446	0.8186	0.8113	0.78285
	1.5	0.8434	-	0.8992	-
	2.0	0.9005	0.9487	0.9444	0.92802
	3.0	0.9567	0.9854	0.9829	0.95930
	4.0	0.9817	0.9989	0.9975	0.99876



All previous calculations have been done with the  $S_{16}$  approximation. This is a rather high approximation which is not necessary in most cases. On table V the escape probabilities of table II have been evaluated as a function of the order of approximation. For practical purpose it is concluded that the approximation  $S_4$  would be sufficient in this case.

It is anticipated that when used with a multigroup thermalization code TIJ would compute the 30-group transport kernels in a time of about one minute (IBM 7094) for a two region cell as above with the approximation  $S_4$ .

Table V

Escape Probabilities Against Order of Approximation  
(see table II)

$\sum_g a$	$S_2$	$S_4$	$S_6$	$S_8$	$S_{12}$	$S_{16}$
0.1	0.8334	0.8204	0.8189	0.8178	0.8166	0.8160
0.3	0.6184	0.5965	0.5946	0.5932	0.5916	0.5908
0.5	0.4869	0.4641	0.4624	0.4611	0.4597	0.4589
0.8	0.3650	0.3446	0.3431	0.3420	0.3407	0.3400
1.0	0.3113	0.2927	0.2913	0.2902	0.2890	0.2884

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# Appendix 1

## Summary of main equations

### 1) Cylindrical geometry

difference equation for boundary values

$$\mu (r_{i+1} \phi_{i+1} - r_i \phi_i) - \frac{r_{i+1} - r_i}{\ell} (\gamma_{m+1} \phi_{m+1} - \gamma_m \phi_m) + \frac{r_{i+1} - r_i}{6} \sum_i \left[ (\ell r_{i+1} + r_i) \phi_i + (\ell r_i + r_{i+1}) \phi_{i+1} \right] = \delta_R \frac{r_{i+1}^2 - r_i^2}{\ell}$$

recursion relation for the coefficients of streaming between rays

$$\gamma_{m+1} - \gamma_m = \ell \mu w \quad (\gamma_0 = 0)$$

linear approximation for the shape of the flux inside a mesh cell

$$\phi_{i+1} + \phi_i = \phi_{m+1} + \phi_m = \ell \bar{\phi}_i$$

$$\begin{array}{lll} i = 1, 2, 3 \dots & I+1 \\ m = 1, 2 \dots & n-2(\ell-1) \\ \ell = 1, 2 \dots & \frac{n}{2} \end{array}$$

for  $m = 0$  the following difference equation is used:

$$\mu (r_{i+1} + r_i) (\phi_{i+1} - \phi_i) + \frac{r_{i+1} - r_i}{6} \sum_i \left[ (\ell r_{i+1} + r_i) \phi_i + (\ell r_i + r_{i+1}) \phi_{i+1} \right] = \delta_R \frac{r_{i+1}^2 - r_i^2}{\ell}$$

and

$$\phi_i + \phi_{i+1} = \ell \phi_{m=0}$$

## 2) Slab geometry

difference equation

$$\mu (\phi_{i+1} - \phi_i) + \frac{\sum_i (x_{i+1} - x_i)(\phi_{i+1} + \phi_i)}{2} = \delta_R (x_{i+1} - x_i)$$

approximation (same as in cylindrical geometry)

$$\begin{aligned} i &= 1, 2 \dots I+1 \\ m &= 1, 2 \dots n \end{aligned}$$

## 3) Both geometries

$$\phi(i) = \sum_{m,p} w \Phi$$

(total flux)

$$P_{R \rightarrow R'} = \frac{1}{V_R} \sum_{i \in R'} (\phi \Sigma_t V)_i$$

(collision probability)

Appendix 2

=====

Input data format

card 1

col 2-72

identification of the problem

card 2

(FORMAT 2413)

col 1-3 (ISN)

n = 2,4,6,8,12 or 16

col 4-6 (IGEOM)

o slab geometry

1 cylindrical geometry

col 7-9 (ICVL)

condition at r (or x) = 0

- cylindrical geometry

o the inner region is a black region

1 reflective condition

- slab geometry

1 reflective condition

2 periodicity condition

col 10-12 (IBVL)

condition at the outer boundary

- cylindrical geometry (r = r<sub>I</sub>)

o the system is in void

1 mirror reflection condition

2 isotropic return along directions of same azimuth

3 isotropic return along all directions

4 arbitrary input law of reflection

- slab geometry

1 mirror reflection (if ICVL = 2 then the periodicity condition is applied)



col 13-15	IAPPT	
16-18	ITSNPT	
19-21	IBVLPT	printing options
22-24	ICVLPT	(see list of symbols in appendix 4)
25-27	ITPT	
28-30	ISNPT	

card 3 (FORMAT 2I3)

col 1-3	(NR)	nb of regions
col 4-6	(NMAT)	nb of cross sections

card 4 (FORMAT 24I3)

col 1-3 etc...	nb of cross section inside each consecutive region
----------------	--

card 5 (FORMAT 6E12.5)

col 1-12 etc...	1	cross section nb 1
	2	" 2
	NMAT	" NMAT

(as much card as necessary)

card 6 (FORMAT 6E12.5)

col 1-12 etc...	$t_1$	thickness of region 1
	$t_2$	" 2
	$t_{NR}$	" NR

(as much card as necessary)

card 7 (FORMAT 6E12.5)

col 1-12	a = 10.0	
13-124	b = 2.0	(see subroutine MESH)
25-36	c = 1.0	

next problem follows

### Appendix 3

#### Sample Problem

The sample problem corresponds to the case calculated by Jonsson<sup>13</sup>  
We consider a three-region system with radii of 1, 2 and 3 mean free path. Results are given in following table.

$P_{ij}$ i j	$T_{ij}$ (IBVL = 2)	Theseus <sup>13</sup>
1 1	0.5915	0.5929
1 2	0.3012	0.3005
1 3	0.0740	0.0732
2 1	0.1002	0.1002
2 2	0.6190	0.6239
2 3	0.2122	0.2112
3 1	0.0148	0.0147
3 2	0.1271	0.1267
3 3	0.6112	0.6168

SAMPLE PROBLEM FOR  
Tij  
(A ONE GROUP TRANSMISSION PROBABILITY  
CODE FOR [REDACTED] CAL ØR [REDACTED]  
GEOMETRIES)

SAMPLE PROBLEM (JONSSON J. OF NUC. EN. VOL 17 P. 515)

16 1 1 0

1

3 1

1 1 1

1.0

1.0

10.0

1.0

2.0

1.0

1.0

CARD

1

2

3

4

5

6

7



\* XEQ

ENTRY POINTS TO SUBROUTINES REQUESTED FROM LIBRARY,  
(FPT) (TSEM) (RTN) (STHM) (FIL)

EXIT

SQRT

EXECUTION  
SAMPLE PROBLEM OF TIJ(A ONE-DIMENSIONAL COLLISION PROBABILITY CODE)

APPROXIMATION S 16

IGEOM= 1

ICVL = 1

IBVL = 0

	THICKNESS	MATERIAL	SIGMA-TOT
	1	2	3
1	0.10000E 01	1	0.10000E 01
2	0.10000E 01	1	
3	0.10000E 01	1	

MATRIX PIJ\*LAMDAJ\*VI

	1	2	3
1	0.29574E-00	0.15061E-00	0.37004E-01
2	0.15031E-00	0.92854E-00	0.31837E-00
3	0.37126E-01	0.31785E-00	0.15279E 01

VOLUME OF REGIONS

	1
1	0.50000E 00
2	0.15000E 01
3	0.25000E 01

COLLISION PROBABILITY MATRIX

	1	2	3
1	0.59148E 00	0.30123E-00	0.74008E-01
2	0.10021E-00	0.61903E 00	0.21224E-00
3	0.14850E-01	0.12714E-00	0.61118E 00

32 LINES OUTPUT THIS JOB.

JOB START AT 20.50  
COMP./LOAD TIME 00.008  
EXECUTION TIME 00.003  
TOTAL JOB TIME 00.011

Appendix 4

=====

List of symbols with printing  
option

Fortran name	Variable name <sup>*</sup> or description	Printing option
DMU (M,L)	(direction cosine)	ISNPT
W (M,L)	w (weight for quadrature)	ISNPT
F(M,L)	Diagonal elements of matrix T (boundary transparency coefficients)	ISNPT
CVL(M,L)	Angular flux at center	ICVLPT
BVL(M,L)	Angular flux at boundary and $\vec{g}_L$ vector components	IBVLPT
PTTP(ML,ML)	Elements of reflection matrix R (directions are ordered like in ref. 2 p. 13)	ISNPT
BVLZW(L)	Angular flux at boundary along $m = 0$ directions (zero weight directions)	IBVLPT
TH(I)	thickness of regions )	always printed
SGT(I)	cross section )	
IMAT(I)	material table ) see input data specifications	
T(I,J)	$P_{R_i \rightarrow R_j}$	ITPT
R(I)	$r_i, x_i$	ITSNPT

<sup>\*</sup>  
refer to text

DR(I)	$r_{i+1} - r_i, \quad x_{i+1} - x_i$	ITSNPT
RM(I)	$\frac{r_{i+1} + r_i}{2}, \quad \frac{x_{i+1} + x_i}{2}$	ITSNPT
V(I)	$\frac{r_{i+1}^2 - r_i^2}{2}, \quad x_{i+1} - x_i$	ITSNPT
VNR(I)	volume of regions	ITSNPT
FMT(I)	$\phi_i$	IAPPT
BM(I)	$\phi_m$	IAPPT
TSN(I)		ISNPT



## Appendix 5

### Description of the subroutines

#### 1) TIJ (main routine)

- read input data
- set up the elements of the R matrix if IBVL  $\neq$  0, 1, 4
- monitor the complete calculation

#### 2) Subroutine CYL (ARG1, ARG2, ARG3)

This routine solves the equations of table I and has two calling sequences:

- a) CALL CYL (IR, ISL, ISR) then an uniform and isotropic source is placed in region IR which means between mesh points  $r_{ISL+1}$  (or  $x_{ISL+1}$ ) and  $r_{ISR}$  (or  $x_{ISR}$ ). The flux is stored in vector TSN (direct transfer) and components of vector g are collected.
- b) CALL CYL (0, IMAXI, IMAXI) then no source is introduced but the boundary flux found in the data block BVL is imposed at the external surface. The flux value are cumulated in TSN (total transfer).

#### 3) Subroutine DMND

From appendix I this subroutine calculates:

- $\phi_i$  function of  $\phi_m, \phi_{i+1}$  for inward directions
- $\phi_{i+1}$  function of  $\phi_m, \phi_i$  for outward directions

#### 4) Subroutine ZWGHT (Y)

is used in cylindrical geometry for the directions ( $m=0$ ) which cross the axis of the cylinder.

$$2 Y = (\phi_i + \phi_{i+1})_{m=0}$$

5) Subroutine BVLCYL

solves the balance equation at the boundary of the lattice cell in cylindrical geometry.

When IBVL is different of 0 or 1, the equation is solved after a fixed number (11) of successive substitutions.

6) Subroutine SLABBC

applies boundary condition on each discrete direction in a slab geometry

7) Subroutine TKRNL(IR)

sets up the collision probability matrix elements when the source region is IR. Also it computes  $\sum_j P_{ij}$  which must sum to one if the boundary la conserves neutrons and is symmetrical.

8) Subroutine SNWGT

prepares  $\mu$  and w for each discrete directions. The three direction cosines are taken from the set of n/2 values.

$$\mu_m^2 = \frac{6m - 5}{3(n-1)} \quad m = 1, 2 \dots \frac{n}{2}$$

The weights are those calculated by Lee<sup>2</sup> using the area method.

9) Subroutine MESH

A fine mesh is automatically prepared. In each region i, the mesh size is  $\lambda_i/A$  with a minimum of B mesh interval in each region (A and B are input data). C is used to modify the mesh size within C mean free path of a boundary.

10) Subroutine MATPT (A, IDIM, JDIM, KDIM, I, J, K)

prints automatically in a suitable form a matrix A with one, two or three dimension (see code for use).

11) Subroutine VCTRPT (N, V1, I1, F1,..., VN, IN, FN)

prints vector of dimension I with variable format

F = 2 (floating point format)

F = 1 (integer point format)

12) Subroutine RLINK

13) Subroutine PRINT

```

* LABEL
CTIJ000
DIMENSION CMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)T1J00001
11,BVLZW(8)T1J00002
DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)T1J00003
DIMENSION R(500),CR(500),V(500),RM(500),SGTH(500),BM(500),FMT(500)T1J00004
11,TSN(500)T1J00005
COMMONICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTCUTT1J00006
COMMONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4T1J00007
COMMONWRK1,WRK2,WRK3,WRK4,CMUML,WML,GMP,GMP1,B1,S
COMMONCMU,W,F,CVL,BVL,PTTP
COMMONTH,SGT,IMAT,NMSH,T
COMMONCR,V,RM,SGTH,V,BM,FMT,TSN,BVLZW
COMMONISNHIC,ISNH1,ISN1,ISNIG,ICVL,IBVL,IBLCK,NRINIT,PI
COMMONIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNPT
NTIN=5
NTOUT=6
PI=3.1415927
10 ISNO=ISNT1J00017
READ INPUT TAPE NTIN,6T1J00018
WRITE OUTPUT TAPE NTCLT,6T1J00019
READINPUTTAPENTIN ,1,ISN,IGEOM,ICVL,IBVL,IAFPT,ITSNPT,IBVLPT,ICVLPT1J00020
11,ITPT,ISNPTT1J00021
WRITE OUTPUT TAPE NTCLT,5,ISN,IGEOM,ICVL,IBVL
IF(ISNO-ISN)15,20,15T1J00022
15 ISNH=ISN/2T1J00023
ISNHIG=ISNH+1+IGEOMT1J00024
ISNH1=ISNH+1T1J00025
ISN1=ISN+1T1J00026
ISNIG=ISN+1+IGEOMT1J00027
ISNHG=ISNH+IGEOMT1J00028
ISNG=ISN+IGEOMT1J00029
CALLSNWCTT1J00030
20 READ INPUT TAPE NTIN,1,NR,NMATT1J00031
READ INPUT TAPE NTIN,1,(IMAT(I),I=1,NR)T1J00032
READ INPUT TAPE NTIN,3,(SGT(I),I=1,NMAT)T1J00033
READ INPUT TAPE NTIN,3,(TH(I),I=1,NR)T1J00034
WRITE OUTPUT TAPE NTCLT,4T1J00035
CALLVCTRPT(3,TH,NR,2,IMAT,NR,1,SGT,NMAT,2)T1J00036
CALLMESH
DC50LC=1,ISNH
DC50MC=1,ISN1
50 F(MC,LC)=0.0T1J00037
IF(IGEOM)300,300,100T1J00038
C CALCULATION OF TRANSPARENCE COEFFICIENTS FOR CYLINDER
100 DC 150 I=1,IMAX1T1J00039
150 TSN(I)=0.0T1J00040
DC8000LC=1,ISNH
J1=ISNHIG-LC
DC8000MC=1,J1T1J00041
8000 BVL(MC,LC)=1.0T1J00042
CALLCYL(0,IMAX1,IMAX1)T1J00043
IF(1BVLPT)8200,8200,8100T1J00044
8100 WRITECUTPUTTAPENTCUT,2001T1J00045
CALL MATPT(PVL,17,8,1,ISN1,ISNH,1)T1J00046
8200 DC8500LC=1,ISNH
F(1,LC)=BVLZW(LC)
J1=ISNHIG-LC
DC8500MC=2,J1
MP=2*J1+1-MC
8500 F(MC,LC)=BVL(MP,LC)T1J00047
IF(1SNPT)8600,8600,8550T1J00048
8550 WRITECUTPUTTAPENTCUT,3000T1J00049
CALL MATPT(F,17,8,1,ISNHG,ISNH,1)T1J00050
8600 K1=ISN*(ISN+2)T1J00051
K1=K1/8T1J00052
IF(1BVL-4)154,152,154T1J00053
154 IF(1BVL-1)370,370,175T1J00054
152 DC 153 K2=1,K1T1J00055
153 READ INPUT TAPE NTIN,3,(PTTP(K2,K),K=1,K1)T1J00056
170 IF(1SNPT)370,370,171T1J00057
171 WRITECUTPUTTAPENTCUT,5000T1J00058
CALLMATPT(PTTP,36,36,1,K1,K1,1)T1J00059
GCTC370T1J00060
175 IF(1BVL-2)959,176,185T1J00061
176 MCLC=0T1J00062
DC180LC=1,ISNH
J2=ISNHIG-LC+1
J3=ISAC-2(LC-1)
WRK1=0.0
DC178MC=J2,J3
178 WRK1=WRK1+W(MC,LC)* CMU(MC,LC)T1J00063
K2=MCLC+1T1J00064
K3=MCLC+ISNH-1-LCT1J00065

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      CC180 MC=J2,J3
      MCLC=MCLC+1
      WML=W(MC,LC)
      DMUML=DMU(MC,LC)
      CC180K=K2,K3
180  PTP(K,MCLC)=DMUML*WML/WRK1
      GCTO170
185  MCLC=0
      WRK1=0.0
      CC180LC=1,ISNH
      J1=ISNH1G-LC
      CC180MC=1,J1
188  WRK1=WRK1+W(MC,LC)*DMU(MC,LC)
      CC190LC=1,ISNH
      J2=ISNH1G-LC+1
      J3=ISNG-2*(LC-1)
      CC190MC=J2,J3
      MCLC=MCLC+1
      WML=W(MC,LC)
      DMUML=DMU(MC,LC)
      CC190K=1,K1
190  PTP(K,MCLC)=DMUML*WML/ABSF(WRK1)
      GCTO170
C    CALCULATION OF TRANSPARENCY COEFFICIENTS FOR SLAB
300  CC355MC=1,ISNH
      DMUML=DMU(MC,1)
      BI=1.0
      CC350I=1,IMAX
      I1=IMAX1-I
350  CALLCMNC
355  F(MC,1)=BI
360  IF(1SNPT)370,370,365
365  WRITECUTPUTTAPENTCUT,3000
      CALLVCTRPT(1,F,ISNH1G,2)
370  CC400I=1,NR
      CC400J=1,NR
400  T(I,J)=0.0
      ISR=0
      ISL=0
      IF(ICVL)410,410,415
410  IF(IGECM)415,415,412
412  NRINIT=2
      GCTO420
415  NRINIT=1
420  CC600IR=NRINIT,NR
      CC450LC=1,ISNH
      CC450MC=1,ISN1
      CVL(MC,LC)=0.0
450  BVL(MC,LC)=0.0
      CC460I=1,IMAX1
460  TSN(I)=0.0
      CTIM=0.0
      ISR=ISR+NMSH(IR)
      ISL=ISL-NMSH(IR)
      CALLCYL(IR,ISL,ISR)
462  CC463LC=1,ISNH
      J1=ISNH1G-LC
      CC4620MC=1,J1
4620 CTIM=CTIM+CVL(MC,LC)*W(MC,LC)*DMU(MC,LC)
      J2=J1+1
      J3=2*J1-IGECM
463  CCNTINLE
464  ISL1=ISL+1
      IF(ITSNPT)470,470,465
465  WRITECUTPUTTAPENTOUT,2000,ISL1,ISR
      WRITECUTPUTTAPENTOUT,2002
      CALLVCTRPT(1,TSN,IMAX1,2)
470  IF(IBVLPT)480,480,475
475  WRITECUTPUTTAPENTOUT,2001
      CALL MATPT(BVL,17,8,1,ISNG,ISNH,1)
480  IF(IGECM)500,500,520
500  CALLSLAEBG
      GCTO560
520  IF(IBVL)550,550,550
550  CALLBVL CYL
560  CALLCYL(0,IMAX1,IMAX1)
562  CC563LC=1,ISNH
      J1=ISNH1G-LC
      CC1562MC=1,J1
1562 CTIM=CTIM+CVL(MC,LC)*W(MC,LC)*DMU(MC,LC)
      J2=J1+1
      J3=2*J1-IGECM
563  CCNTINLE
2563 IF(ICVL)564,564,564

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1563	WRITE CLTPUT TAPE 6,5001,CTIM	TIJ00167
564	IF(ITSNPT)570,570,565	TIJ00168
565	WRITECUTPUTTAPENTOUT,2000,ISL1,ISR	TIJ00169
	WRITECUTPUTTAPENTOUT,2003	TIJ00170
	CALLVCTRPT(1,TSN,IMAX1,2)	TIJ00171
570	IF(1BVLP1)580,580,575	TIJ00172
575	WRITECUTPUTTAPENTOUT,2001	TIJ00173
	CALLMATFT(1BVL,17, 8,1,ISNG,ISNH,1)	TIJ00174
580	CALLTKRNL(IR)	TIJ00175
600	CONTINUE	TIJ00176
999	GOTO10	TIJ00177
	1 FCRMAT(2413)	TIJ00178
	3 FCRMAT(6E12.5)	TIJ00179
	4 FCRMAT(1H09X37HTHICKNESS MATERIAL SIGMA-TOT)	TIJ00180
	5 FCRMAT (16H0APPROXIMATION S,13/7H0IGECM=13/7H0ICVL =13/7H01BVL =13/7H01BVL)	TIJ00181
	1)	TIJ00182
	6 FCRMAT (72H	TIJ00183
	1 )	TIJ00184
2000	FCRMAT(1H08X11HSOURCE(I)=1/10X3H(I=12,1F,12,1F))	TIJ00185
2002	FCRMAT(1H07X1SHDIRECT TR.COE.)	TIJ00186
2001	FCRMAT(23H0BOUNDARY VALLES MATRIX)	TIJ00187
2003	FCRMAT(1H07X14HTOTAL TR.COE.)	TIJ00188
3000	FCRMAT(35H0BOUNDARY TRANSPARENCE COEFFICIENTS)	TIJ00189
4001	FCRMAT(1H0)	TIJ00190
5000	FCRMAT(18H0REFLECTION MATRIX)	TIJ00191
5001	FCRMAT (27HCCURRENT AT BLACK BOUNDARY=E12.5)	TIJ00192
	END	TIJ00193
*	LABEL	
CCYL000		CYL00000
	SLBROUTINECYL(IR,ISL,ISR)	CYL00001
	DIMENSION CMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),FTTP(36,36)	CYL00002
	1),BVLZW(8)	CYL00003
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	CYL00004
	DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),RM(500),FMT(500)	CYL00005
	1),TSN(500)	CYL00006
	COMMONICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	CYL00007
	COMMONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	CYL00008
	COMMONWRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,RI,S	CYL00009
	COMMONCMU,W,F,CVL,BVL,PTTP	CYL00010
	COMMONTH,SGT,IMAT,NMSH,T	CYL00011
	COMMONCR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW	CYL00012
	COMMONISNHIC,ISNH1,ISN1,ISN1G,ICVL,1BVL,IPLCK,NRINIT,PI	CYL00013
	COMMONIAFPT,ITSNPT,1BVLP1,ICVLP1,ITPT,ISNPT	CYL00014
	DC4COLC=1,ISNH	CYL00015
	DC20I=1,IMAX1	CYL00016
	BM(1)=0.0	CYL00017
20	FMT(1)=0.0	CYL00018
	GMP=0.0	CYL00019
	GMP1=0.0	CYL00020
C	INWARD DIRECTIONS MESH SWEEP	CYL00021
	J1=ISNHIG-LC	CYL00022
	DC2COMC=1,J1	CYL00023
	WML=W(MC,LC)	CYL00024
	DMUML=CMU(MC,LC)	CYL00025
75	IF(1GECM)85,85,80	CYL00026
80	GMP=GMP1	CYL00027
	GMP1=CMF1-2.0*WML*DMUML	CYL00028
85	IF(1R)9C,90,99	CYL00029
90	BI=BVL(MC,LC)	CYL00030
	IM=IMAX	CYL00031
	GCTC150	CYL00032
99	BI=0.0	CYL00033
	IM=IMAX	CYL00034
100	TSN(IM+1)=TSN(IM+1)+WML*BI	CYL00035
	FMT(IM+1)=BI	CYL00036
	DC150I=1,IM	CYL00037
	I1=IM-I+1	CYL00038
	I2=I1	CYL00039
	IF(I1-ISL)110,110,113	CYL00040
113	IF(I1-ISR)112,112,110	CYL00041
112	S=1.0	CYL00042
	GCTC115	CYL00043
110	S=0.0	CYL00044
115	IF(WML)120,120,130	CYL00045
120	CALLZKGT(Y)	CYL00046
	BM(1)=Y	CYL00047
	GCTC150	CYL00048
130	CALLCMND	CYL00049
	TSN(I2)=TSN(I2)+WML*FMT(I2)	CYL00050
150	CONTINUE	CYL00051
152	IF(1AFPT)19C,190,155	CYL00052
155	WRITECUTPUTTAPENTOUT,1000,MC,LC	CYL00053
	CALLVCTRPT(2,FMT,IMAX1,2,BM,IMAX,2)	CYL00054
190	CVL(MC,LC)=BI	CYL00055

192 IF(IWML)1920,1920,194	CYL00056
1920 IF(ICVL)1921,1921,1930	CYL00057
1921 BI=0.0	CYL00058
1930 CC196011=1,IMAX	CYL00059
I2=11+1	CYL00060
IF(I1-ISL)1950,1950,1935	CYL00061
1935 IF(I1-ISR)1940,1940,1950	CYL00062
1940 S=1.0	CYL00063
GCTC1955	CYL00064
1950 S=0.0	CYL00065
1955 CALLZWCHT(Y)	CYL00066
FMT(11)=Y	CYL00067
1960 CCNTINUE	CYL00068
BVLZW(LC)=B1	CYL00069
IF(IAFPT)200,200,1961	CYL00070
1961 WRITECUTPUTTAPENTOUT,4000	CYL00071
CALLVCTRPT(1,FMT,IMAX,2)	CYL00072
GCTC200	CYL00073
194 IF(IGECM)200,200,195	CYL00074
195 MF=2*J1+1-MC	CYL00075
IF(ICVL)196,196,197	CYL00076
196 CVL(MP,LC)=C.0	CYL00077
GOTC200	CYL00078
197 CVL(MP,LC)=F1	CYL00079
200 CCNTINUE	CYL00080
260 J2=J1+1	CYL00081
J3=2*J1-IGECM	CYL00082
CC390MC=J2,J3	CYL00083
WML=W(MC,LC)	CYL00084
DMUML=CMU(MC,LC)	CYL00085
264 IF(IGECM)265,265,270	CYL00086
265 IF(IR1275,275,267	CYL00087
267 BI=C.C	CYL00088
IMIN=ISL+1	CYL00089
GCTC280	CYL00090
270 GMP=GMP1	CYL00091
GMP1=CMF1-2.0*WML*DMUML	CYL00092
275 IMIN=1	CYL00093
BI=CVL(MC,LC)	CYL00094
280 TSN(IMIN)=TSN(IMIN)+WML*BI	CYL00095
FMT(IMIN)=B1	CYL00096
CC35011=IMIN,IMAX	CYL00097
I2=11+1	CYL00098
304 IF(I1-ISL)320,320,305	CYL00099
305 IF(I1-ISR)310,310,320	CYL00100
310 S=1.0	CYL00101
GCTC330	CYL00102
320 S=0.0	CYL00103
330 CALLOMNC	CYL00104
335 TSN(I2)=TSN(I2)+WML*FMT(I2)	CYL00105
350 CCNTINUE	CYL00106
356 IF(IAFPT)380,380,357	CYL00107
357 WRITECUTPUTTAPENTOUT,1000,MC,LC	CYL00108
CALLVCTRPT(2,FMT,IMAX1,2,8M,IMAX,2)	CYL00109
380 BVL(MC,LC)=B1	CYL00110
390 CCNTINUE	CYL00111
IF(IGECM)410,410,400	CYL00112
400 CCNTINUE	CYL00113
J1=ISNH	CYL00114
GCTO415	CYL00115
410 J1=1	CYL00116
415 IF(ICVLFT)450,450,420	CYL00117
420 WRITECUTPUTTAPENTOUT,2000	CYL00118
CALLMATPT(CVL,17,8,1,ISN1,J1,1)	CYL00119
450 IF(IBVLFT)460,460,455	CYL00120
455 WRITECUTPUTTAPENTOUT,3000	CYL00121
CALLVCTRPT(1,BVLZW,ISNH,2)	CYL00122
460 RETURN	CYL00123
1000 FORMAT(1H013X12HANGULAR FLUX/14X4H (M=12,4H,L= 12,1H)/1H011X3H NI1C	CYL00124
11X4HNM+1)	CYL00125
2000 FORMAT(22HOCENTRAL VALUES MATRIX)	CYL00126
3000 FORMAT(28H0ZERO WEIGHT BOUNCARY VALUES//)	CYL00127
4000 FORMAT(20HORADIAL OUTWARD FLUX//)	CYL00128
END	CYL00129
* LABEL	
CCMND00	CMND0000
SUBROUTINECMND	CMND0001
DIMENSION CMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),FTTP(36,36	CMND0002
1),BVLZW(8)	CMND0003
DIMENSION TH(20),SGT(20),IMAT(20),NMSP(20),T(20,20)	CMND0004
DIMENSION R(500),CR(500),V(500),RV(500),SCTHV(500),BM(500),FMT(500	CMND0005
1),TSN(500)	CMND0006
COMMONIGECM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	CMND0007
CCPMONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	CMND0008

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      CCMONCNRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,BI,S
      CCMONCDMU,W,F,CVL,BVL,PTTP
      CCMONCTH,SGT,IMAT,NMST,T
      CCMONDR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW
      CCMONISNHIG,ISNH1,ISN1,ISN1G,ICVL,IBVL,IBLCK,NRINIT,PI
      CCMONIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNFT
50  IF(IGECM)220,220,100
C  CALCULATES ANGULAR TERMS FOR CYLINDER
100  BM11=BM(11)
      WRK3=CR(11)/WML/2.0
      WRK2=CMP1*WRK3
      WRK1=(CMP+GMP1)*WRK3*BM11/2.0
      WRK4=SGTHV(11)/(6.0*RM(11))
120  FM=(S*V(11)/2.0+BI*(ABSF(DMLML)*RM(11)+SIGNF(CR(11),CMUML)*WRK4)
      +WRK1)/(4.0*WRK4*RM(11)+(ABSF(DMUML)+2.0*WRK4)*R(12)+WRK2)
      BM(11)=2.0*FM-BM11
200  BI=2.0*FM-BI
      FMT(12)=BI
210  RETURN
220  FM=(S*V(11)/2.0+ABSF(DMUML)*BI)/(SGTHV(11)+ABSF(DMUML))
      GCTC2CC
      END
      LABEL
* CZWGHTO
      SLBROUTINEZWGHT(BM11)
      DIMENSION CMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)
      1),BVLZW(8)
      DIMENSION TH(20),SGT(20),IMAT(20),NMST(20),T(20,20)
      DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500)
      1),TSN(500)
      CCMONICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT
      CCMONCK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4
      CCMONCNRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,BI,S
      CCMONCDMU,W,F,CVL,BVL,PTTP
      CCMONCTH,SGT,IMAT,NMST,T
      CCMONDR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW
      CCMONIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNFT
      DMUML=CMU(MC,LC)
      WRK1=ABSF(DMUML)*RM(11)
      WRK2=0.33333*SGTHV(11)/RM(11)
      WRK3=BI
      OBI=(S*V(11)+(WRK1-WRK2*(4.*RM(11)-R(12)))*BI)/
      1(WRK1+WRK2*(2.0*RM(11)+R(12)))
      BM11=(WRK3+BI)/2.0
      RETURN
      END
      LABEL
* CBVLCYO
      SLBROUTINEBVLCYL
      DIMENSION DMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)
      1),BVLZW(8)
      DIMENSION TH(20),SGT(20),IMAT(20),NMST(20),T(20,20)
      DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500)
      1),TSN(500)
      CCMONICEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT
      CCMONCK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4
      CCMONCNRK1,WRK2,WRK3,WRK4,DMUML,WML,GMP,GMP1,BI,S
      CCMONCDMU,W,F,CVL,BVL,PTTP
      CCMONCTH,SGT,IMAT,NMST,T
      CCMONDR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW
      CCMONISNHIG,ISNH1,ISN1,ISN1G,ICVL,IBVL,IBLCK,NRINIT,PI
      CCMONIAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNFT
      ISN1=ISN+1
      DC1COLC=1,ISNH
      J1=ISNHIG-LC
      DC1COMC=1,J1
100  CVL(MC,LC)=C.0
      IF(1BVL-1)145,110,145
110  DC135LC=1,ISNH
      J1=ISNHIG-LC
      DC130MC=2,J1
      MP=2*J1+1-MC
130  BVL(MC,LC)=BVL(MP,LC)/(1.0-F(MC,LC))
135  BVL(1,LC)=BVLZW(LC)/(1.0-F(1,LC))
      GC TO 3C0
145  K1=ISN*(ISN+2)
      K1=K1/8
      DC250NIT=1,10
      DC160LC=1,ISNH
      J1=ISNHIG-LC
      J2=2*J1-IGECM
      J3=J1+1
      DC150MC=J3,J2
      MP=2*J1+1-MC

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CMND0009
CMND0010
CMND0011
CMND0012
CMND0013
CMND0014
CMND0015
CMND0016
CMND0017
CMND0018
CMND0019
CMND0020
CMND0021
CMND0022
CMND0023
CMND0024
CMND0025
CMND0026
CMND0027
CMND0028
CMND0029
CMND0030
ZWGHT000
ZWGHT001
ZWGHT002
ZWGHT003
ZWGHT004
ZWGHT005
ZWGHT006
ZWGHT007
ZWGHT008
ZWGHT009
ZWGHT010
ZWGHT011
ZWGHT012
ZWGHT013
ZWGHT014
ZWGHT015
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ZWGHT018
ZWGHT019
ZWGHT020
ZWGHT021
ZWGHT022
BVLCY000
BVLCY001
BVLCY002
BVLCY003
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BVLCY027
BVLCY028
BVLCY029
BVLCY030
BVLCY031
BVLCY032
BVLCY033
BVLCY034
BVLCY035
BVLCY036

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150	F(MC,LC)=BVL(MC,LC)*BVL(MP,LC)*F(MP,LC)	BVLCY037
160	CONTINUE	BVLCY038
	MCLC=0	BVLCY039
	DC220LC=1, ISNH	BVLCY040
	J1=ISNH1G-LC	BVLCY041
	DC210MC=2, J1	BVLCY042
	MCLC=MCLC+1	BVLCY043
	LP=1	BVLCY044
	K2=0	BVLCY045
	WRK1=0.0	BVLCY046
	CC200K=1, K1	BVLCY047
	K2=K2+1	BVLCY048
	IF (ISNH-LP+1-K2) 180, 190, 190	BVLCY049
180	K2=1	BVLCY050
	LP=LP+1	BVLCY051
190	MP=K2+ISNH1G-LP	BVLCY052
200	WRK1=WRK1+PTTP(MCLC,K)*F(MP,LP)	BVLCY053
210	BVL(MC,LC)=WRK1	BVLCY054
220	BVL(1,LC)=BVL(2,LC)	BVLCY055
	IF (IBVLPT) 250, 250, 225	BVLCY056
225	WRITECUTPUTTAPENTOUT, 1000, NIT	BVLCY057
	CALL MATPT(BVL, 17, 8, 1, ISN1, ISNH, 1)	BVLCY058
250	CONTINUE	BVLCY059
	IF (ITSNPT) 255, 300, 255	BVLCY060
255	WRITECUTPUTTAPENTOUT, 1000, NIT	BVLCY061
	CALL MATPT(BVL, 17, 8, 1, ISN1, ISNH, 1)	BVLCY062
300	RETURN	BVLCY063
1000	FORMAT(29H08BOUNDARY VALUES MATRIX ,NIT=12)	BVLCY064
	END	BVLCY065
	LABEL	
CSLBBEC		SLABBC00
	SLBROUTINESLABBC	SLABBC01
	DIMENSION DMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)	SLABBC02
	1),BVLZW(8)	SLABBC03
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	SLABBC04
	DIMENSION R(500),DR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500)	SLABBC05
	1),TSN(500)	SLABBC06
	COMMON GEOM, ISN, ISNH, MC, LC, NR, IMAX, IMAX1, ATIN, NTOUT	SLABBC07
	COMMON K1, K2, K3, K4, J1, J2, J3, J4, I1, I2, I3, I4	SLABBC08
	COMMON WRK1, WRK2, WRK3, WRK4, DMUML, WML, GMP, GMP1, B1, S	SLABBC09
	COMMON CMU, W, F, CVL, BVL, PTTP	SLABBC10
	COMMON TH, SGT, IMAT, NMSH, T	SLABBC11
	COMMON DR, V, RM, SGTHV, BM, FMT, TSN, BVLZW	SLABBC12
	COMMON ISNH1G, ISNH1, ISN1, ISN1G, ICVL, IBVL, IELCK, NRINIT, PI	SLABBC13
	COMMON IAFPT, ITSNPT, IBVLPT, ICVLPT, ITPT, ISNPT	SLABBC14
500	IF (ICVL-1) 530, 520, 505	SLABBC15
C	PERIODIC SLAB	SLABBC16
505	DC510MC=1, ISNH	SLABBC17
	BVL(MC,1)=CVL(MC,1)/(1.0-F(MC,1))	SLABBC18
	MP=ISN1-MC	SLABBC19
510	CVL(MP,1)=BVL(MP,1)/(1.0-F(MC,1))	SLABBC20
	GCTC560	SLABBC21
C	REFLECTIVE SLAB	SLABBC22
520	DC525MC=1, ISNH	SLABBC23
	MP=ISN1-MC	SLABBC24
	CVL(MP,1)=(CVL(MC,1)*F(MC,1)+BVL(MP,1))/(1.0-F(MC,1)*.2)	SLABBC25
525	BVL(MC,1)=(BVL(MP,1)+F(MC,1)*CVL(MC,1))/(1.0-F(MC,1)*.2)	SLABBC26
	GCTC560	SLABBC27
C	BLACK INNER CONDITION	SLABBC28
530	DC535MC=1, ISNH	SLABBC29
	MP=ISN1-MC	SLABBC30
	CVL(MP,1)=0.0	SLABBC31
535	BVL(MC,1)=BVL(MP,1)	SLABBC32
560	RETURN	SLABBC33
	END	SLABBC34
	LABEL	
CTKRNL0		TKRNL001
	SLBROUTINETKRNL(IR)	TKRNL002
	DIMENSION DMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36)	TKRNL003
	1),BVLZW(8)	TKRNL004
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	TKRNL005
	DIMENSION R(500),DR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500)	TKRNL006
	1),TSN(500)	TKRNL007
	COMMON GEOM, ISN, ISNH, MC, LC, NR, IMAX, IMAX1, ATIN, NTOUT	TKRNL008
	COMMON K1, K2, K3, K4, J1, J2, J3, J4, I1, I2, I3, I4	TKRNL009
	COMMON WRK1, WRK2, WRK3, WRK4, DMUML, WML, GMP, GMP1, B1, S	TKRNL010
	COMMON CMU, W, F, CVL, BVL, PTTP	TKRNL011
	COMMON TH, SGT, IMAT, NMSH, T	TKRNL012
	COMMON DR, V, RM, SGTHV, BM, FMT, TSN, BVLZW	TKRNL013
	COMMON ISNH1G, ISNH1, ISN1, ISN1G, ICVL, IBVL, IELCK, NRINIT, PI	TKRNL014
	COMMON IAFPT, ITSNPT, IBVLPT, ICVLPT, ITPT, ISNPT	TKRNL015
	DIMENSION VNR(20)	TKRNL016
	IF (ICVL) 45, 45, 50	TKRNL017
45	NRINIT=2	

	GCTC55	TKRNL018
50	NRINIT=1	TKRNL019
55	K1=NRINIT	TKRNL020
	K2=NMSH(K1)	TKRNL021
	DC110I=1,IMAX	TKRNL022
	IF(1-K2)100,100,90	TKRNL023
90	K1=K1+1	TKRNL024
	K2=K2+NMSH(K1)	TKRNL025
100	IF(IGECM)105,105,108	TKRNL026
105	T(IR,K1)=T(IR,K1)+0.5*DR(I)*(TSN(I)+TSN(I+1))	TKRNL027
	GCTC110	TKRNL028
108	T(IR,K1)=T(IR,K1)+DR(I)*(TSN(I+1)*(2.0*R(I+1)+R(I))+TSN(I)*(2.0*	TKRNL029
	IR(I)+R(I+1)))/6.0	TKRNL030
110	CONTINUE	TKRNL031
160	IF(IR-NR)200,650,200	TKRNL032
650	IF(ITPT)655,200,655	TKRNL033
655	J2=0	TKRNL034
	WRITE OUTPUT TAPE NTOUT,3000	TKRNL035
	CALLMATPT(T,20,20,1,NR,NR,1)	TKRNL036
	DC660I=NRINIT,NR	TKRNL037
	J1=J2+1	TKRNL038
	J2=J2+NMSH(I)	TKRNL039
	VNR(I)=0.0	TKRNL040
	DC660J=J1,J2	TKRNL041
660	VNR(I)=VNR(I)+V(J)	TKRNL042
	WRITECUTPUTTAPENTOUT,4000	TKRNL043
	CALLVCTRPT(1,VNR,NR,2)	TKRNL044
	DC680I=NRINIT,NR	TKRNL045
	WRK1=0.0	TKRNL046
	DC670J=NRINIT,NR	TKRNL047
	K2=IMAT(J)	TKRNL048
	T(I,J)=SGT(K2)*T(I,J)/VNR(I)	TKRNL049
670	WRK1=WRK1+T(I,J)	TKRNL050
	IF(1BV)200,680,675	TKRNL051
675	WRITE OUTPUT TAPE NTOUT,1000,1,WRK1	TKRNL052
680	CONTINUE	TKRNL053
	WRITECUTPUTTAPENTOUT,2000	TKRNL054
	CALLMATPT(T,20,20,1,NR,NR,1)	TKRNL055
200	RETURN	TKRNL056
1000	FCRMT(16HOSUM OVER J OF P,13,4H J=E12.5)	TKRNL057
2000	FCRMT(29HOCOLLISION PROBABILITY MATRIX)	TKRNL058
3000	FCRMT(21HCMATRIX PIJ=LAMDAJ*VI//)	TKRNL059
4000	FCRMT(18HOVOLUME OF REGIONS)	TKRNL060
	END	TKRNL061
	LABEL	
CMESH=CO		MESH0000
	SLBROUTINEMESH	MESH0001
	DIMENSION DMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36	MESH0002
	1),BVLZW(8)	MESH0003
	DIMENSION TH(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	MESH0004
	DIMENSION R(500),DR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500	MESH0005
	1),TSN(500)	MESH0006
	COMMONICEOM,ISN,ISNH,PC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	MESH0007
	COMMONK1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	MESH0008
	COMMONWRK1,WRK2,WRK3,WRK4,CMUML,WML,GMP,GMP1,B1,S	MESH0009
	COMMONCMU,W,F,CVL,BVL,PTTP	MESH0010
	COMMONTH,SGT,IMAT,NMSH,T	MESH0011
	COMMONR,DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW	MESH0012
	COMMONISNHIC,ISNH1,ISN1,ISN1G,ICVL,1BVL,1BLCK,NRINIT,PI	MESH0013
	COMMONIAFPT,ITSNPT,1BVLPT,ICVLPT,ITPT,ISNPT	MESH0014
	DIMENSIONBMSH(20),CMST(20)	MESH0015
	READ INPUT TAPE 5,1004,A,B,C	MESH0016
	BMSH=500	MESH0017
	IF(IGECM)75,75,50	MESH0018
50	IF(ICVL)60,60,75	MESH0019
60	NRINIT=2	MESH0020
	R(1)=TH(1)	MESH0021
	GCTC80	MESH0022
75	NRINIT=1	MESH0023
	R(1)=0.0	MESH0024
80	DC130K1=NRINIT,NR	MESH0025
	WRK1=TH(K1)	MESH0026
	K2=IMAT(K1)	MESH0027
	WRK2=1./SGT(K2)	MESH0028
	WRK3=WRK2/A	MESH0029
	WRK4=WRK1/B	MESH0030
	IF(WRK3-WRK4)100,110,110	MESH0031
100	CMST(K1)=WRK3	MESH0032
	GCTC115	MESH0033
110	CMST(K1)=WRK4	MESH0034
115	WRK3=WRK2/C	MESH0035
	WRK4=WRK1/2.	MESH0036
	IF(WRK3-WRK4)120,130,130	MESH0037
120	BMSH(K1)=WRK3	MESH0038

130	GCTC131	MESH0039
131	BMSH(K1)=WRK4	MESH0040
	IMSH=1	MESH0041
	XR2=R(1)	MESH0042
	YR2=CMST(INRINIT)	MESH0043
	XR1=XR2	MESH0044
	YR1=YR2	MESH0045
	X=R(1)	MESH0046
	DRC=CMST(INRINIT)	MESH0047
	CC260K=NRINIT,NR	MESH0048
	K2=0	MESH0049
	K3=IMAT(K)	MESH0050
	XL1=XR1	MESH0051
	XL2=XR2	MESH0052
	YL1=YR1	MESH0053
	YL2=YR2	MESH0054
	WRK1=R(IMSH)	MESH0055
	WRK2=WRK1+T*(K)	MESH0056
	IF(K-NR)135,1352,1352	MESH0057
135	YR1=YR2	MESH0058
	YR2=CMST(K+1)	MESH0059
	IF(YR2-YR1)1351,1352,1353	MESH0060
1351	XR1=WRK2-BMSH(K)	MESH0061
	XR2=WRK2	MESH0062
	GCTC137	MESH0063
1352	XR1=WRK2	MESH0064
	XR2=WRK2	MESH0065
	GCTC137	MESH0066
1353	XR1=WRK2	MESH0067
	XR2=WRK2+BMSH(K+1)	MESH0068
137	K1=1	MESH0069
140	IMST=IMSH	MESH0070
	IMST=IMSH+1	MESH0071
	IF(IMSHX-IMSH)270,270,145	MESH0072
145	K2=K2+1	MESH0073
	IF(X-XL2)15C,170,17C	MESH0074
150	DRC=RLINK(XL1,YL1,XL2,YL2,X)	MESH0075
	GCTC250	MESH0076
170	IF(X-XR1)175,175,190	MESH0077
175	IF(XR1-WRK2)180,176,190	MESH0078
176	IF(X-XR1+0.2*DRC)180,210,210	MESH0079
180	DRC=CMST(K)	MESH0080
	GCTC250	MESH0081
190	IF(X-WRK2+0.2*DRC)200,210,210	MESH0082
200	DRC=RLINK(XR1,YR1,XR2,YR2,X)	MESH0083
	GCTC250	MESH0084
210	X=WRK2	MESH0085
	IMSH=IMSH	MESH0086
	IMSH=IMSH-1	MESH0087
	DRC=X-R(IMST)	MESH0088
	K1=2	MESH0089
	K2=K2-1	MESH0090
	GCTC251	MESH0091
250	X=X+DRC	MESH0092
251	R(IMST-1)=X	MESH0093
	WRK3=(R(IMST-1)+R(IMSH))/2.0	MESH0094
	IF(IGEOM)253,253,254	MESH0095
253	V(IMSH)=DRC	MESH0096
	GCTC255	MESH0097
254	V(IMST)=DRC*WRK3	MESH0098
255	RM(IMSH)=WRK3	MESH0099
	SGTHV(IMSH)=SGT(K3)*V(IMSH)/2.	MESH0100
	DR(IMSH)=DRC	MESH0101
	GCTC(14C,257),K1	MESH0102
257	NMSH(K)=K2	MESH0103
260	CCNTINUE	MESH0104
	IMAX=IMSH	MESH0105
	IMAX1=IMSH1	MESH0106
	IF(ITSNFT)265,265,262	MESH0107
262	WRITECUTPUTTAPENTOUT,1002	MESH0108
	WRITECUTPUTTAPENTOUT,1003	MESH0109
	OCALLPRINT(8,R,IMAX1,2,DR,IMAX,2,RP,IMAX,2,V,IPAX,2,NMSH,NR,1,CMST,	MESH0110
	INR,2,BMSH,NR,2,SGTHV,IMAX,2)	MESH0111
265	RETURN	MESH0112
270	WRITECUTPUTTAPE6,1001	MESH0113
	CALLEXIT	MESH0114
1001	FCRMT(21H TOO MUCH MESH POINTS)	MESH0115
1002	FCRMT(1H151X16HGEOMETRICAL MESH//)	MESH0116
1003	FCRMT(///11X6HRACTUSEX6HCELTAR6HREPEAN6HVOLUME//)	MESH0117
1004	FCRMT(3E12,5)	MESH0118
	END	MESH0119
	LABEL	
* CRLINK0	FLNCTICARLINK(X1,Y1,X2,Y2,X)	RLINK000
		RLINK001



CSNWGT0	SLBROUTINESNWGT	SNWGT000
	SN DIRECTICA MESH AND WEIGHTS FOR N=2,4,6,8,120R16	SNWGT001
C	DIMENSION CMU(17,8),W(17,8),F(17,8),CVL(17,8),BVL(17,8),PTTP(36,36	SNWGT002
	1),BVLZW(8)	SNWGT003
	DIMENSION T(20),SGT(20),IMAT(20),NMSH(20),T(20,20)	SNWGT004
	DIMENSION R(500),CR(500),V(500),RM(500),SGTHV(500),BM(500),FMT(500	SNWGT005
	1),TSN(500)	SNWGT006
	COMMON GEOM,ISN,ISNH,MC,LC,NR,IMAX,IMAX1,NTIN,NTOUT	SNWGT007
	COMMON K1,K2,K3,K4,J1,J2,J3,J4,I1,I2,I3,I4	SNWGT008
	COMMON WRK1,WRK2,WRK3,WRK4,CMUML,WML,GMP,GMP1,B1,S	SNWGT009
	COMMON CMU,W,F,CVL,BVL,PTTP	SNWGT010
	COMMON T,SGT,IMAT,NMSH,T	SNWGT011
	COMMON DR,V,RM,SGTHV,BM,FMT,TSN,BVLZW	SNWGT012
	COMMON ISNH1G,ISNH1,ISN1,ISN1G,ICVL,IBVL,IBLCK,NRINIT,PI	SNWGT013
	COMMON IAFPT,ITSNPT,IBVLPT,ICVLPT,ITPT,ISNPT	SNWGT014
	DIMENSION P(8)	SNWGT015
	X\$ABF(1)=2*K3+1-I+2*IGE	SNWGT016
	X\$AMF(1)=K3+1-I+2*IGE	SNWGT017
	XTBCF(1)=K3+1	SNWGT018
15	IF(IGECM)16,16,17	SNWGT019
16	IGE=0	SNWGT020
	GCTC18	SNWGT021
17	IGE=1	SNWGT022
18	ISNH=ISN/2	SNWGT023
	ISNH1=ISNH+1	SNWGT024
	ISN1=ISN+1	SNWGT025
	ISNH1G=ISNH+1+IGE	SNWGT026
	ISN1G=ISN+1+IGE	SNWGT027
	ISNH1G=ISNH+IGE	SNWGT028
	ISNG=ISN+IGE	SNWGT029
	CC150J=1,ISNH	SNWGT030
	CC150I=1,ISN1	SNWGT031
	W(I,J)=0.0	SNWGT032
150	CMU(I,J)=0.0	SNWGT033
	IF(ISNH-912C0,555,555	SNWGT034
C	PREPARATION OF COSML	SNWGT035
200	CC260 L=1,ISNH	SNWGT036
	J1=ISNH1-L	SNWGT037
	CC250 M=1,J1	SNWGT038
	K=J1+1-M	SNWGT039
	MC=M+IGE	SNWGT040
	X=(6.*FLOATF(K)-5.)/(3.*(FLOATF(ISN)-1.))	SNWGT041
	X=-SQRTF(X)	SNWGT042
	CMU(MC,L)=X	SNWGT043
210	K=2*J1+1-M+IGE	SNWGT044
	DMU(K,L)=-X	SNWGT045
250	CCNTINUE	SNWGT046
	IF(IGECM)260,270,255	SNWGT047
255	CMU(1,L)=-SQRTF(1.-CMU(MD,1)**2)	SNWGT048
260	CCNTINUE	SNWGT049
270	GCTC(300,310,320,330,555,350,555,370),ISNH	SNWGT050
C	S2 WEIGHTS	SNWGT051
300	P(1)=0.5	SNWGT052
	GCTC500	SNWGT053
C	S4 WEIGHTS	SNWGT054
310	P(1)=0.16666667	SNWGT055
	GCTC500	SNWGT056
C	S6 WEIGHTS	SNWGT057
320	P(1)=0.08043063	SNWGT058
	P(2)=0.08623605	SNWGT059
	GCTC500	SNWGT060
C	S8 WEIGHTS	SNWGT061
330	P(1)=0.05330038	SNWGT062
	P(2)=0.05058636	SNWGT063
	P(3)=0.03658070	SNWGT064
	GCTC500	SNWGT065
C	S12 WEIGHTS	SNWGT066
350	P(1)=0.03188428	SNWGT067
	P(2)=0.02844993	SNWGT068
	P(3)=0.02268799	SNWGT069
	P(4)=0.01736872	SNWGT070
	P(5)=0.01513782	SNWGT071
	GCTC500	SNWGT072
C	S16 WEIGHTS	SNWGT073
370	P(1)=0.02275580	SNWGT074
	P(2)=0.01988730	SNWGT075
	P(3)=0.01502308	SNWGT076
	P(4)=0.01366597	SNWGT077
	P(5)=0.01164258	SNWGT078
	P(6)=0.00931431	SNWGT079
	P(7)=0.00881570	SNWGT080
	P(8)=0.00767130	SNWGT081
500	J3=0	SNWGT082
		SNWGT083



	CC530 L=1, ISNH	SNWGT084
	J1=ISNH-1-L	SNWGT085
	J2=J1/2	SNWGT086
	IF(J1-2*J2)503,503,502	SNWGT087
502	J2=J2+1	SNWGT088
503	CC520 M=1, J2	SNWGT089
	M=M	SNWGT090
	MC=M+IGE	SNWGT091
	IF(W(MC,L))520,510,520	SNWGT092
510	J3=J3+1	SNWGT093
	X=P(J3)	SNWGT094
	K2=0	SNWGT095
511	K2=K2+1	SNWGT096
	GCTO(5111,5113,5115,520),K2	SNWGT097
5111	MP=M+IGE	SNWGT098
	LF=L	SNWGT099
	GCTO513	SNWGT100
5113	LP=M	SNWGT101
	GCTC512	SNWGT102
5115	LP=J1+1-M	SNWGT103
512	MP=L+IGE	SNWGT104
513	K1=0	SNWGT105
	MC=MP	SNWGT106
	K3=ISNH-1-LP	SNWGT107
514	K1=K1+1	SNWGT108
	W(MP,LP)=X	SNWGT109
	GCTC(515,516,517,511),K1	SNWGT110
515	MP=XSABF(MC)	SNWGT111
	GCTO514	SNWGT112
516	MP=XSAMF(MC)	SNWGT113
	GCTC514	SNWGT114
517	MF=XTRCF(MC)	SNWGT115
	GCTC514	SNWGT116
520	CONTINUE	SNWGT117
530	CONTINUE	SNWGT118
	IF(IGECM)540,531,540	SNWGT119
531	CC538M=2, ISNH	SNWGT120
	WRK1=C.C	SNWGT121
	CC535L=2,M	SNWGT122
	MC=M-L+1	SNWGT123
	WRK1=WRK1+W(MC,L)	SNWGT124
	W(MC,L)=0.0	SNWGT125
	DMU(MC,L)=0.0	SNWGT126
	K3=ISNH-1-L	SNWGT127
	MP=XSABF(MC)	SNWGT128
	W(MP,L)=0.0	SNWGT129
535	DMU(MP,L)=0.0	SNWGT130
	W(M,1)=W(M,1)+WRK1	SNWGT131
	MP=ISNH-M	SNWGT132
538	W(MP,1)=W(M,1)	SNWGT133
540	IF(ISNPT)543,543,542	SNWGT134
542	WRITECLPUTTAPENTOLT,1000,ISN	SNWGT135
	CC545LC=1, ISNH	SNWGT136
	J1=ISN-2*(LC-1)+IGE	SNWGT137
	WRITECUTPUTTAPENTOUT,1001,(M,LC,DMU(M,LC),W(M,LC),M=1,J1)	SNWGT138
543	IF(IGECM)545,550,545	SNWGT139
545	CONTINUE	SNWGT140
550	RETURN	SNWGT141
555	WRITECLPUTTAPENTOUT,1002,ISN	SNWGT142
	CALLEXIT	SNWGT143
1000	FCRMT(1H149X19HANGULAR SN MESH (N=12,1F))//45X3HPML10X4HPML11X3HWSN	SNWGT144
	1ML//)	SNWGT145
1001	FCRMT(44X11P212,3X2E14.5)	SNWGT146
1002	FCRMT(25H SN WEIGHTS ARE NOT PROVIDED FOR N=[4]	SNWGT147
	END	SNWGT148
•	LABEL	
CPRINT0		PRINT000
	SUBROUTINEPRINT(NITEM,V1,L1,IT1,V2,L2,IT2,V3,L3,IT3,V4,L4,IT4,V5,L	PRINT001
	15,IT5,V6,L6,IT6,V7,L7,IT7,V8,L8,IT8)	PRINT002
	DIMENSIONV1(1),V2(1),V3(1),V4(1),V5(1),V6(1),V7(1),V8(1)	PRINT003
	DIMENSIONFORMAT(9),VLIN(E)	PRINT004
C	BUILT-IN FORMATS	PRINT005
	FCRMT(1)=6F(2X14,	PRINT006
	FMTFX1=6H7X,17,	PRINT007
	FMTFX2=6H7X,17)	PRINT008
	FMTFL1=6HE14.5,	PRINT009
	FMTFL2=6HE14.5)	PRINT010
	FMTBK1=6H13XA1,	PRINT011
	FMTBK2=6H13XA1)	PRINT012
B	BLANK=6C606C606060	PRINT013
	WRITE CLPUT TAPE 6,1000,(1,I=1,NITEM)	PRINT014
	LINC=0	PRINT015
S	K=0	PRINT016
C	FCRMT CF LINE	PRINT017

```

      LINC=LINC+1
      CC2501=1,NITEM
      GCTC(10,20,30,40,50,60,70,80),I
10  ITYPE=IT1
      LENGTH=L1
B   VAR=V1(LINC)
      GCTC10C
20  ITYPE=IT2
      LENGTH=L2
B   VAR=V2(LINC)
      GCTC10C
30  ITYPE=IT3
      LENGTH=L3
B   VAR=V3(LINC)
      GCTC10C
40  ITYPE=IT4
      LENGTH=L4
B   VAR=V4(LINC)
      GCTC10C
50  ITYPE=IT5
      LENGTH=L5
B   VAR=V5(LINC)
      GCTC10C
60  ITYPE=IT6
      LENGTH=L6
B   VAR=V6(LINC)
      GCTC10C
70  ITYPE=IT7
      LENGTH=L7
B   VAR=V7(LINC)
      GCTC10C
80  ITYPE=IT8
      LENGTH=L8
B   VAR=V8(LINC)
100 IF(LINC-LENGTH)150,150,200
150 GCTC(116C,17C),ITYPE
160 IF(I-8)162,165,165
162 FMT=FMTEFX1
      GCTC20C
165 FMT=FMTEFX2
      GCTC20C
170 IF(I-8)172,175,175
172 FMT=FMTEFL1
      GCTC20C
175 FMT=FMTEFL2
      GCTC20C
200 K=K+1
      IF(I-8)202,205,205
202 FMT=FMTEK1
      GCTC20C
205 FMT=FMTEK2
207 VAR=BLANK
208 FCRMAT(I+1)=FMT
      VLINE(I)=VAR
      MF=I
250 CCNTINUE
      IF(MP-8)260,280,2E0
260 MP=MP+1
      CC2701=MP,8
      FCRMAT(I+1)=FMTEBK1
270 VLINE(I)=BLANK
      FCRMAT(5)=FMTEBK2
280 IF(K-NITEM)300,290,290
290 RETURN
300 WRITEOUTPUTTAPE6,FORMAT,LINC,(VLINE(I),I=1,8)
      GCTO5
1000 FCRMAT(1H013X11,7I14)
      END

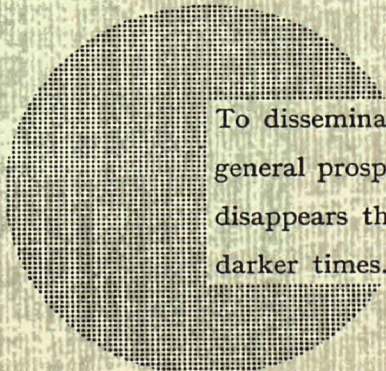
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PRINT018
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To disseminate knowledge is to disseminate prosperity — I mean general prosperity and not individual riches — and with prosperity disappears the greater part of the evil which is our heritage from darker times.

Alfred Nobel



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